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In[386]:= dNdξ[ξ_, η_] := { $\frac{1}{4}(-1 + \eta)$ ,  $\frac{1 - \eta}{4}$ ,  $\frac{1 + \eta}{4}$ ,  $\frac{1}{4}(-1 - \eta)$ };
dNdη[ξ_, η_] := { $\frac{1}{4}(-1 + \xi)$ ,  $\frac{1}{4}(-1 - \xi)$ ,  $\frac{1 + \xi}{4}$ ,  $\frac{1 - \xi}{4}$ };

computeBandJ[defPos_, ξ_, η_] := Module[{X, Y, j11, j12, j21,
  j22, detJ, Jinv11, Jinv12, Jinv21, Jinv22, Jmat, Nmat, Dmat, B},

  X = defPos[[1]];
  Y = defPos[[2]];

  j11 = X.dNdξ[ξ, η];
  j12 = Y.dNdξ[ξ, η];
  j21 = X.dNdη[ξ, η];
  j22 = Y.dNdη[ξ, η];

  detJ = j11 j22 - j12 j21;

  Jinv11 = j22 / detJ;
  Jinv12 = -j12 / detJ;
  Jinv21 = -j21 / detJ;
  Jinv22 = j11 / detJ;

  Dmat = {{1.0, 0, 0, 0}, {0, 0, 0, 1.0}, {0, 1.0, 1.0, 0}};

  Jmat = {{Jinv11, Jinv12, 0, 0},
    {Jinv21, Jinv22, 0, 0}, {0, 0, Jinv11, Jinv12}, {0, 0, Jinv21, Jinv22}};

  Nmat = {Riffle[dNdξ[ξ, η], {0, 0, 0, 0}], Riffle[dNdη[ξ, η], {0, 0, 0, 0}],
    Riffle[{0, 0, 0, 0}, dNdξ[ξ, η]], Riffle[{0, 0, 0, 0}, dNdη[ξ, η]]};

  B = Dmat.Jmat.Nmat;

  Return[{B, detJ}]
];

computeYieldFunction[Y_, H_, β_, pressure_, ep_] := Module[{hard},

  hard = Y + H ep;

  Return[Sqrt[2. / 3.] (β pressure + hard)]
];

computeNormalDirection[Sij_, S_, β_] := Module[{k, temp, mag},

  temp =  $\frac{3}{2}$  Sqrt[ $\frac{2}{3}$ ]  $\frac{Sij}{s}$  +  $\frac{1}{3}$  β IdentityMatrix[3];

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mag = Sqrt[Sum[temp[[i, j]] temp[[i, j]], {i, 1, 3}, {j, 1, 3}]];

Return[temp / mag]
]

computeStress[σn_, Δd_, B_, EY_, ν_, Y_, H_, β_, ep_, stepNPlasticFlag_] :=
Module[{Δε, Cmat, σtr, Str, S, K, Pnpl, onpl, temp, Δεkk, Δεδ, Sn, SnMag, Sij, μ,
  pressure, Δλ, Qij, ΔS, x, Snpl, Δep, σzz, σzzN, stepNPlPlasticFlag, ΔεδQij},

  (*Compute strain increment*)
  Δε = B.Flatten[Δd];

  (*Compute an elastic trial stress (plane strain)*)
  Cmat = 
$$\frac{E_Y}{(1. + \nu) (1. - 2. \nu)}$$
 {{(1 - ν), ν, 0}, {ν, (1 - ν), 0}, {0, 0, (1. - 2. ν)}}};

  σtr = σn + Cmat.Δε;

  (*from Hooke's law and the plane strain condition, σzz*)
  σzzE = ν (σtr[[1]] + σtr[[2]]);

  (*Compute deviatoric trial stress and switch to tensor notation*)
  Str = {{σtr[[1]], σtr[[3]], 0}, {σtr[[3]], σtr[[2]], 0}, {0, 0, σzzE}} -

$$\frac{1}{3} (\sigma_{tr}[[1]] + \sigma_{tr}[[2]] + \sigma_{zzE}) \text{IdentityMatrix}[3];$$


  (*Compute deviatoric trial stress magnitude*)
  S = Sqrt[Sum[Str[[i, j]] Str[[i, j]], {i, 1, 3}, {j, 1, 3}]];

  (*σzz under plastic loading that is consistent with normality rule*)
  σzzP = 
$$\frac{1}{2} \left( (\sigma_{tr}[[1]] + \sigma_{tr}[[2]]) + \frac{\sqrt{3} \beta \sqrt{(9 - \beta^2) (4 \sigma_{tr}[[3]]^2 + (\sigma_{tr}[[1]] - \sigma_{tr}[[2]])^2)}}{\beta^2 - 9} \right);$$


  (*this is the effective pressure at the yield surface,
  the σzz term comes from enforcing the plastic z-
  direction strains are 0 under the normality condition*)
  pressure = 
$$-\frac{1}{3} (\sigma_{tr}[[1]] + \sigma_{tr}[[2]] + \sigma_{zzP});$$


  (*Check for yielding*)
  If[Re[S] ≤ Re[computeYieldFunction[Y, H, β, pressure, ep]],
    (*not yielding, trial stress is new stress*)
    onpl = σtr;
    Δep = 0;
    stepNPlPlasticFlag = 0,
    (*else, possibly yielding*)

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(*compute dilatation increment*)

$$\Delta\epsilon_{kk} = \frac{1}{3} (\Delta\epsilon[[1]] + \Delta\epsilon[[2]]);$$

(*compute deviatoric strain increment*)

$$\Delta\epsilon_d = \{\{\Delta\epsilon[[1]], \Delta\epsilon[[3]], 0\}, \{\Delta\epsilon[[3]], \Delta\epsilon[[2]], 0\}, \{0, 0, 0\}\} - \Delta\epsilon_{kk} \text{IdentityMatrix}[3];$$

(*compute old deviatoric stress (at step N)*)

$$\text{Sn} = \{\{\sigma_n[[1]], \sigma_n[[3]], 0\}, \{\sigma_n[[3]], \sigma_n[[2]], 0\}, \{0, 0, \sigma_{zzE}\}\} - \frac{1}{3} (\sigma_n[[1]] + \sigma_n[[2]] + \sigma_{zzE}) \text{IdentityMatrix}[3];$$

(*Deviatoric stress magnitude at step N*)

$$\text{SnMag} = \text{Sqrt}[\text{Sum}[\text{Sn}[[i, j]] \text{Sn}[[i, j]], \{i, 1, 3\}, \{j, 1, 3\}]];$$



$$\mu = \frac{E\gamma}{2(1+\nu)};$$


(*recompute the "trial" deviatoric stress with the plastic  $\sigma_{zz}$  term*)

$$\text{Str} = \{\{\sigma_{tr}[[1]], \sigma_{tr}[[3]], 0\}, \{\sigma_{tr}[[3]], \sigma_{tr}[[2]], 0\}, \{0, 0, \sigma_{zzP}\}\} - \frac{1}{3} (\sigma_{tr}[[1]] + \sigma_{tr}[[2]] + \sigma_{zzP}) \text{IdentityMatrix}[3];$$

(*Compute deviatoric trial stress magnitude*)

$$\text{S} = \text{Sqrt}[\text{Sum}[\text{Str}[[i, j]] \text{Str}[[i, j]], \{i, 1, 3\}, \{j, 1, 3\}]];$$



$$Q_{ij} = \text{computeNormalDirection}[\text{Str}, \text{S}, \beta];$$



$$\Delta\epsilon_d Q_{ij} = \text{Sum}[\Delta\epsilon_d[[i, j]] Q_{ij}[[i, j]], \{i, 1, 3\}, \{j, 1, 3\}];$$


(*compute for  $\Delta\lambda$ *)

$$\Delta\lambda = \frac{3 \left( \sqrt{6} \text{SnMag} - 2\gamma - 2 \text{pressure} \beta - 2 H \epsilon_p + 4 \Delta\epsilon_d Q_{ij} \mu \right)}{2 \left( \sqrt{6} H + 6 \mu \right)};$$


(*Determine if yielding*)
If[Re[ $\Delta\lambda$ ]  $\leq 0.$ ,
  (*not yielding, trial stress is new stress*)
   $\sigma_{npl} = \sigma_{tr};$ 
   $\Delta\epsilon_p = 0.$ ;
  stepNP1PlasticFlag = 0,
  (*yielding*)

  (*update deviatoric stress*)

   $\text{Snpl} = \text{computeYieldFunction}[\gamma, H, \beta, \text{pressure}, \epsilon_p + \text{Sqrt}[2/3] \Delta\lambda] * Q_{ij};$ 

  (*update stress vector*)
   $\sigma_{npl} = \{\text{Snpl}[[1, 1]], \text{Snpl}[[2, 2]], \text{Snpl}[[1, 2]]\} - \text{pressure} * \{1, 1, 0\};$ 
   $\Delta\epsilon_p = \text{Sqrt}[2/3] \Delta\lambda;$ 
  stepNP1PlasticFlag = 1
];
];
```

```

Return[{ $\sigma_{np1}$ ,  $\Delta\epsilon$ ,  $\Delta\epsilon_p$ , stepNP1PlasticFlag}]
];

computeForce[defPos_, disp_, Ey_,  $\nu$ _, Y_, H_,  $\beta$ _,  $\epsilon_{p1}$ _,
   $\epsilon_{p2}$ _,  $\epsilon_{p3}$ _,  $\epsilon_{p4}$ _,  $\sigma_{1n}$ _,  $\sigma_{2n}$ _,  $\sigma_{3n}$ _,  $\sigma_{4n}$ _, stepNPlasticFlag1_,
  stepNPlasticFlag2_, stepNPlasticFlag3_, stepNPlasticFlag4_] :=
Module[{B1, B2,  $\sigma_2$ , B3, B4, J1, J2, J3, J4,  $\sigma_{1np1}$ ,  $\sigma_{2np1}$ ,  $\sigma_{3np1}$ ,  $\sigma_{4np1}$ ,
   $\Delta\epsilon_1$ ,  $\Delta\epsilon_2$ ,  $\Delta\epsilon_3$ ,  $\Delta\epsilon_4$ ,  $\Delta\epsilon_{p1}$ ,  $\Delta\epsilon_{p2}$ ,  $\Delta\epsilon_{p3}$ ,  $\Delta\epsilon_{p4}$ , stepNP1PlasticFlag1,
  stepNP1PlasticFlag2, stepNP1PlasticFlag3, stepNP1PlasticFlag4},

{B1, J1} = computeBandJ[defPos, -Sqrt[1 / 3.], -Sqrt[1 / 3.]];
{ $\sigma_{1np1}$ ,  $\Delta\epsilon_1$ ,  $\Delta\epsilon_{p1}$ , stepNP1PlasticFlag1} =
  computeStress[ $\sigma_{1n}$ , disp, B1, Ey,  $\nu$ , Y, H,  $\beta$ ,  $\epsilon_{p1}$ , stepNPlasticFlag1];

{B2, J2} = computeBandJ[defPos, -Sqrt[1 / 3.], Sqrt[1 / 3.]];
{ $\sigma_{2np1}$ ,  $\Delta\epsilon_2$ ,  $\Delta\epsilon_{p2}$ , stepNP1PlasticFlag2} =
  computeStress[ $\sigma_{2n}$ , disp, B2, Ey,  $\nu$ , Y, H,  $\beta$ ,  $\epsilon_{p2}$ , stepNPlasticFlag2];

{B3, J3} = computeBandJ[defPos, Sqrt[1 / 3.], -Sqrt[1 / 3.]];
{ $\sigma_{3np1}$ ,  $\Delta\epsilon_3$ ,  $\Delta\epsilon_{p3}$ , stepNP1PlasticFlag3} =
  computeStress[ $\sigma_{3n}$ , disp, B3, Ey,  $\nu$ , Y, H,  $\beta$ ,  $\epsilon_{p3}$ , stepNPlasticFlag3];

{B4, J4} = computeBandJ[defPos, Sqrt[1 / 3.], Sqrt[1 / 3.]];
{ $\sigma_{4np1}$ ,  $\Delta\epsilon_4$ ,  $\Delta\epsilon_{p4}$ , stepNP1PlasticFlag4} =
  computeStress[ $\sigma_{4n}$ , disp, B4, Ey,  $\nu$ , Y, H,  $\beta$ ,  $\epsilon_{p4}$ , stepNPlasticFlag4];

Return[{B1T. $\sigma_{1np1}$  J1 + B2T. $\sigma_{2np1}$  J2 + B3T. $\sigma_{3np1}$  J3 + B4T. $\sigma_{4np1}$  J4,  $\sigma_{1np1}$ ,  $\sigma_{2np1}$ ,
   $\sigma_{3np1}$ ,  $\sigma_{4np1}$ ,  $\Delta\epsilon_1$ ,  $\Delta\epsilon_2$ ,  $\Delta\epsilon_3$ ,  $\Delta\epsilon_4$ ,  $\Delta\epsilon_{p1}$ ,  $\Delta\epsilon_{p2}$ ,  $\Delta\epsilon_{p3}$ ,  $\Delta\epsilon_{p4}$ , stepNP1PlasticFlag1,
  stepNP1PlasticFlag2, stepNP1PlasticFlag3, stepNP1PlasticFlag4}]

];

computeTangentStiffness[defPos_, disp_, Ey_,  $\nu$ _, Y_, H_,  $\beta$ _,  $\epsilon_{p1}$ _,  $\epsilon_{p2}$ _,
   $\epsilon_{p3}$ _,  $\epsilon_{p4}$ _,  $\sigma_1$ _,  $\sigma_2$ _,  $\sigma_3$ _,  $\sigma_4$ _, stepNPlasticFlag1_, stepNPlasticFlag2_,
  stepNPlasticFlag3_, stepNPlasticFlag4_] := Module[{h, k},

h = 1  $\times$  10-50;

k = Map[computeForce[defPos, Partition[#, 2], Ey,  $\nu$ , Y, H,  $\beta$ ,  $\epsilon_{p1}$ ,  $\epsilon_{p2}$ ,  $\epsilon_{p3}$ ,  $\epsilon_{p4}$ ,  $\sigma_1$ ,
   $\sigma_2$ ,  $\sigma_3$ ,  $\sigma_4$ , stepNPlasticFlag1, stepNPlasticFlag2, stepNPlasticFlag3,
  stepNPlasticFlag4][[1] &, IdentityMatrix[2 Length[nodes]] * I h];

Return[-Im[kT] / h]

];

In[394]:= (*Setup problem*)
nodes = {{0.0, 0.0}, {1.0, 0.0}, {1.0, 1.0}, {0.0, 1.0}};
disp = ConstantArray[{0.0, 0.0}, Length[nodes]];

```

```

defPos = nodes;
Ey = 200;
v = 0.29;
Y = 15;
H = 0;
β = 0.0;
εpn = 0.0;
σ1n = {0., 0., 0.};
σ2n = {0., 0., 0.};
σ3n = {0., 0., 0.};
σ4n = {0., 0., 0.};
ε1 = {0., 0., 0.};
ε2 = {0., 0., 0.};
ε3 = {0., 0., 0.};
ε4 = {0., 0., 0.};
ep1 = 0.;
ep2 = 0.;
ep3 = 0.;
ep4 = 0.;
stepNPlasticFlag1 = 0;
stepNPlasticFlag2 = 0;
stepNPlasticFlag3 = 0;
stepNPlasticFlag4 = 0;

stressStrain = {{{0., 0., 0.}, {0., 0., 0.}}};

(*Begin load stepping iteration*)
Do[

  PrintTemporary["Load Step = ", i];

  (*Apply the initial kinematic BC's*)
  disp = ConstantArray[{0.0, 0.0}, Length[nodes]];
  disp[[2]] += {-0.005, 0.0};
  disp[[3]] += {-0.005, 0.0};

  (*Begin Newton iteration*)
  Do[

    (*Calculate the total force*)
    {f, σ1np1, σ2np1, σ3np1, σ4np1, Δε1,
     Δε2, Δε3, Δε4, Δep1, Δep2, Δep3, Δep4, stepNP1PlasticFlag1,
     stepNP1PlasticFlag2, stepNP1PlasticFlag3, stepNP1PlasticFlag4} =
    computeForce[defPos, disp, Ey, v, Y, H, β, ep1, ep2, ep3, ep4, σ1n, σ2n, σ3n, σ4n,
     stepNPlasticFlag1, stepNPlasticFlag2, stepNPlasticFlag3, stepNPlasticFlag4];

    (*Zero residual on boundary condition nodes,
    they are supposed to have reaction forces*)
    f[{{1, 2, 3, 4, 5, 7}}] = {0.0, 0.0, 0.0, 0.0, 0.0, 0.0};

    (*Compute residual*)
    res = Norm[f];

    PrintTemporary[" Residual = ", res];
  ];
];

```

```

(*Break if convergence achieved*)
If[res < 0.0000001, Break[]];

(*Compute tangent stiffness*)

K = Chop[computeTangentStiffness[defPos, disp, Ey,  $\nu$ ,
  Y, H,  $\beta$ ,  $\epsilon_1$ ,  $\epsilon_2$ ,  $\epsilon_3$ ,  $\epsilon_4$ ,  $\sigma_{1n}$ ,  $\sigma_{2n}$ ,  $\sigma_{3n}$ ,  $\sigma_{4n}$ , stepNPlasticFlag1,
  stepNPlasticFlag2, stepNPlasticFlag3, stepNPlasticFlag4]];

(*Apply essential BC's to tangent stiffness*)
K[[1]] = Normal@SparseArray[1  $\rightarrow$  1, 2 * Length[nodes]];
K[[2]] = Normal@SparseArray[2  $\rightarrow$  1, 2 * Length[nodes]];
K[[3]] = Normal@SparseArray[3  $\rightarrow$  1, 2 * Length[nodes]];
K[[4]] = Normal@SparseArray[4  $\rightarrow$  1, 2 * Length[nodes]];
K[[5]] = Normal@SparseArray[5  $\rightarrow$  1, 2 * Length[nodes]];
K[[7]] = Normal@SparseArray[7  $\rightarrow$  1, 2 * Length[nodes]];

(*Solve the linear problem for a displacement increment*)
disp += Partition[LinearSolve[K, f], 2];

, {j, 0, 50}
];

(*Update the deformed position and stresses with the converged results*)
defPos += disp;
 $\sigma_{1n}$  =  $\sigma_{1np1}$ ;
 $\sigma_{2n}$  =  $\sigma_{2np1}$ ;
 $\sigma_{3n}$  =  $\sigma_{3np1}$ ;
 $\sigma_{4n}$  =  $\sigma_{4np1}$ ;
 $\epsilon_1$  +=  $\Delta\epsilon_1$ ;
 $\epsilon_2$  +=  $\Delta\epsilon_2$ ;
 $\epsilon_3$  +=  $\Delta\epsilon_3$ ;
 $\epsilon_4$  +=  $\Delta\epsilon_4$ ;
 $\epsilon_1$  +=  $\Delta\epsilon_1$ ;
 $\epsilon_2$  +=  $\Delta\epsilon_2$ ;
 $\epsilon_3$  +=  $\Delta\epsilon_3$ ;
 $\epsilon_4$  +=  $\Delta\epsilon_4$ ;
stepNPlasticFlag1 = stepNP1PlasticFlag1;
stepNPlasticFlag2 = stepNP1PlasticFlag2;
stepNPlasticFlag3 = stepNP1PlasticFlag3;
stepNPlasticFlag4 = stepNP1PlasticFlag4;

AppendTo[stressStrain, { $\sigma_{3n}$ ,  $\epsilon_3$ }]

, {i, 50}
]

```

In[421]:= Graphics[{{Dashed, Line[{nodes[[1]], nodes[[2]], nodes[[3]], nodes[[4]], nodes[[1]]]}}, {Line[{defPos[[1]], defPos[[2]], defPos[[3]], defPos[[4]], defPos[[1]]}}}]

Out[421]=



```
In[422]:= stress = stressStrain[[All, 1]][[All, 1]];
strain = stressStrain[[All, 2]][[All, 1]];
```

```
ListLinePlot[{-strain, -stress}^T]
```

Out[424]=

