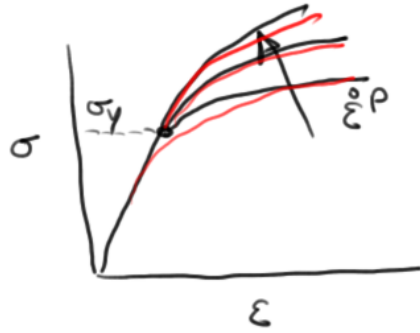


Viscoplastic



$$f = \sqrt{\frac{3}{2}} S - \sigma_y (1 + \beta \dot{\epsilon}^p)^N$$

$$\dot{f} = 0$$

$$0 = \sqrt{\frac{3}{2}} \dot{S} - N \sigma_y \beta \ddot{\epsilon}^p (1 + \beta \dot{\epsilon}^p)^{N-1} \quad \dot{\epsilon}^p = \dot{\lambda} S_{ij}$$

$$= \sqrt{\frac{3}{2}} \dot{S} - \sqrt{\frac{2}{3}} N \sigma_y \beta \ddot{\lambda} (1 + \beta \sqrt{\frac{2}{3}} \dot{\lambda})^{N-1}$$

$$\dot{S} = \frac{2}{3} N \sigma_y \beta \ddot{\lambda} (1 + \beta \sqrt{\frac{2}{3}} \dot{\lambda})^{N-1} \Rightarrow \star$$

$$0 = \dot{m}_{ij} Q_{ij} - \frac{1}{3M} N \sigma_y \ddot{\lambda} (1 + \beta \sqrt{\frac{2}{3}} \dot{\lambda})^{N-1} - \dot{\lambda}$$

$$f(J_2) = \sqrt{3J_2} - Y(\epsilon_p, \dot{\epsilon}_p)$$

Other yield surfaces

Maximum shear stress (Tresca Criterion)

$$f = \frac{1}{2} \max \left\{ |\sigma_I - \sigma_{II}|, |\sigma_{II} - \sigma_{III}|, |\sigma_I - \sigma_{III}| \right\}$$

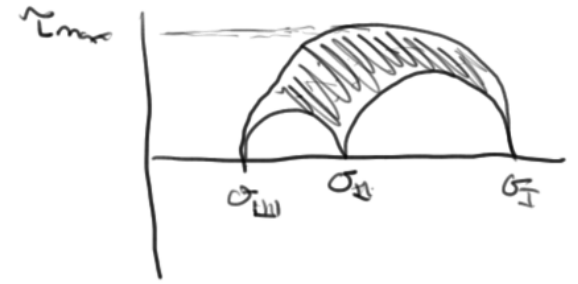
$$= 4J_2^3 - \underbrace{27J_3^2} - 9J_2^2 + Y - 6J_2Y^4 - Y^6 = 0$$

$$J_3 = \det(S_{ij}) = \sigma_I^3 \sigma_{II}^3 \sigma_{III}^3$$

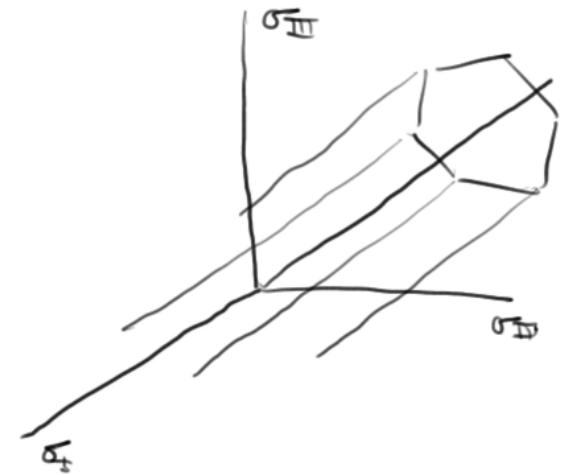
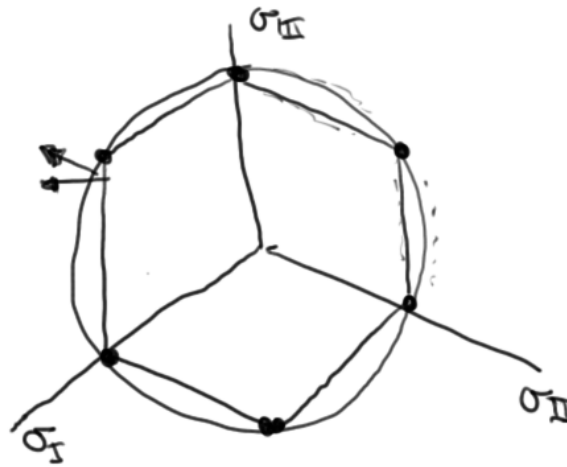
$$S_{ij} = \begin{bmatrix} -\frac{2}{3}Y & 0 & 0 \\ 0 & +\frac{1}{3}Y & 0 \\ 0 & 0 & +\frac{1}{3}Y \end{bmatrix}$$

$$J_3 = \frac{2}{27} Y^3 \quad \text{tension}$$

$$J_3 = -\frac{2}{27} Y^3 \quad \text{compression}$$



(Lubliner)



Drucker - Prager

$$f(p, J_2) = \sqrt{3J_2} - \underbrace{\beta p} - Y(\epsilon^p, \dot{\epsilon}^p, T) = 0$$

$$p = -\frac{1}{3} \sigma_{kk}$$

$$\frac{\partial f}{\partial \sigma_{ij}} \Rightarrow \beta \frac{\partial p}{\partial \sigma_{ij}} = \frac{\partial}{\partial \sigma_{ij}} \left(-\frac{1}{3} \sigma_{kk} \right) \beta = -\frac{1}{3} \delta_{ik} \delta_{jk} \beta = -\frac{1}{3} \delta_{ij} \beta$$

pressure dep. in
the plastic flow
rule
↓

Mohr - Coulomb

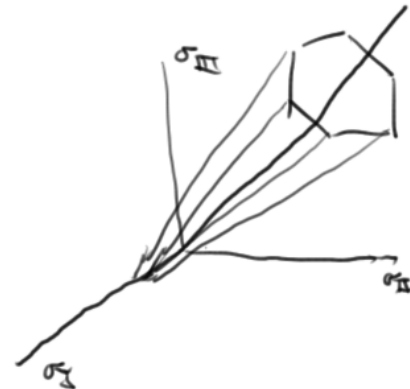
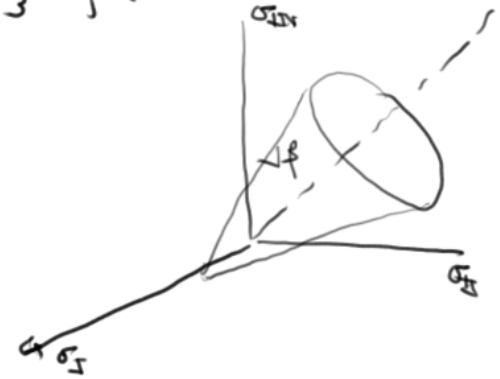
$$\sigma_I - \sigma_{III} + (\sigma_I + \sigma_{III}) \sin(\phi) = Y \cos(\phi)$$

In terms of the invariants

↖ angle of internal friction

$$\frac{1}{3} I_I \sin \phi + \sqrt{J_2} \left\{ \cos \theta - \frac{1}{\sqrt{3}} \sin \theta \sin \phi \right\} = \frac{Y}{2} \cos(\phi)$$

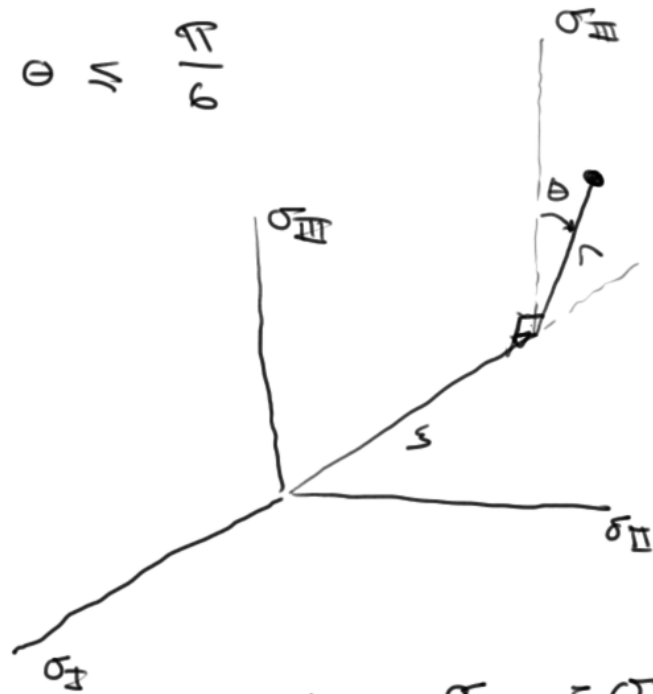
$\theta \rightarrow$ Lode angle



Lode angle

$$\Theta = \frac{1}{3} \sin^{-1} \left(\frac{3\sqrt{3}}{2} \frac{J_3}{J_2^{3/2}} \right)$$

$$-\frac{\pi}{6} \leq \Theta \leq \frac{\pi}{6}$$



$$\sigma_I = \sigma_{II} = \sigma_{III}$$

Θ is controlled by the relationship of the intermediate principle stresses, i.e. σ_I to $\sigma_{II}, \sigma_{III}$

$$\text{When } \sigma_{II} = \sigma_{III} \Rightarrow \Theta = 60^\circ$$

$$\sigma_{II} = \sigma_I \Rightarrow \Theta = 0^\circ$$