

$$\frac{d}{dt} (ds)^2 = d\vec{x}^T \left( 2 \frac{dE}{dt} \right) d\vec{x}$$

$$d\vec{x} = F d\vec{X}$$

$$\begin{aligned} \frac{d}{dt} (ds)^2 &= d\vec{x}^T (2D) d\vec{x} \\ &= (F d\vec{X})^T (2D) (F d\vec{X}) \\ &= d\vec{X}^T \left[ F^T (2D) F \right] d\vec{X} \end{aligned}$$

$$d\vec{x}^T (2D) d\vec{x} = 2 \frac{d\vec{x}^T (L^T e + \dot{e} + eL) d\vec{x}}{2}$$

$$D = L^T e + \dot{e} + eL$$

$$\boxed{\frac{dE}{dt} = F^T D F} \rightarrow \text{rate-of-green strain}$$

Eulerian strain rate

$$\begin{aligned} \frac{d}{dt} (ds)^2 &= \frac{d}{dt} \left( d\vec{x}^T (2e) d\vec{x} \right) \\ &= 2 \left[ (L d\vec{x})^T e d\vec{x} + d\vec{x}^T \frac{de}{dt} d\vec{x} + d\vec{x}^T e (L d\vec{x}) \right] \\ &= 2 \underbrace{d\vec{x}^T (L^T e + \dot{e} + eL) d\vec{x}}_{2D} \end{aligned}$$

$$\boxed{\dot{e} = D - L^T e - eL} \rightarrow \text{rate-of-Eulerian strain}$$

Stress (Heuristic argument)

$$P(i) = \frac{dw}{dt} = \int \vec{F} \cdot \frac{d\vec{v}}{dt} \left( \frac{dv}{dV} \right)$$

$$\begin{aligned} &= \int \frac{f_i}{A_j} \frac{dv_i}{dx_j} dV \\ &= \int \sigma : L dV \\ \sigma : L &= \sigma_{ij} L_{ij} \end{aligned}$$

$$\int \sigma : (D + W) dV$$

$$P = \int \sigma : D dV$$

$\vec{x} = \vec{x}(\vec{X}, t) \rightarrow$  "current" configuration

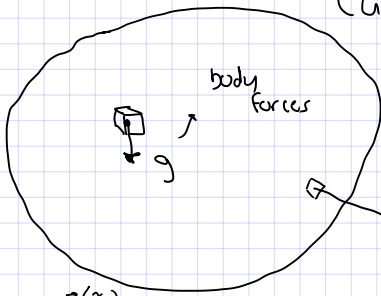
$$dv = \vec{A} d\vec{x} = A_j dx_j$$

$$L = \text{symm}(L) + \text{antisymm}(L)$$

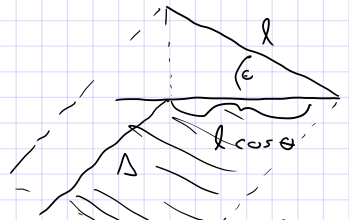
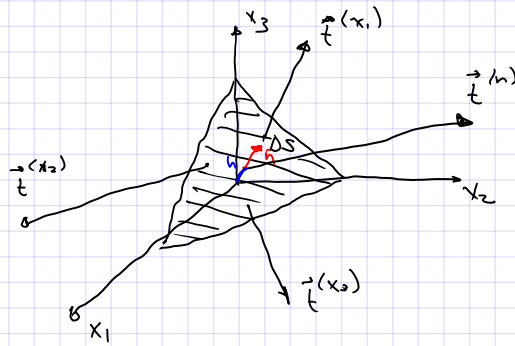
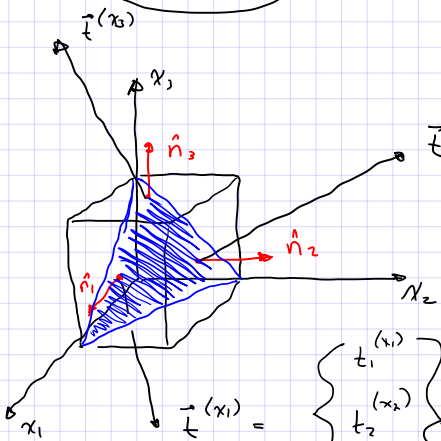
$$= \underbrace{\frac{1}{2} (L^T + L)}_D + \underbrace{\frac{1}{2} (L - L^T)}_W$$

$$\sigma : W = \vec{0}$$

# Current



surface forces  $\rightarrow$  tractions  $\rightarrow$   $\frac{\text{force}}{\text{area}}$



$$\hat{n} = \begin{cases} \cos(\hat{n}, x_1) \rightarrow n_1 \\ \cos(\hat{n}, x_2) \rightarrow n_2 \\ \cos(\hat{n}, x_3) \rightarrow n_3 \end{cases} \quad \text{A case}$$

$$\vec{t} = \begin{cases} t_1(x_1) \\ t_2(x_2) \\ t_3(x_3) \end{cases}$$

$\lim_{h \rightarrow 0}$

$$\Sigma F = \vec{t}^{(n)} \Delta S - \vec{t}^{(x_2)} n_2 \Delta S - \vec{t}^{(x_3)} n_3 \Delta S - \vec{t}^{(x_1)} n_1 \Delta S = \rho \frac{1}{3} h \Delta S \vec{g}$$

$$\vec{t}^{(n)} = \vec{t}^{(x_1)} n_1 + \vec{t}^{(x_2)} n_2 + \vec{t}^{(x_3)} n_3$$

$$\vec{t}^{(n)T} = \vec{t}^{(x_1)T} n_1 + \vec{t}^{(x_2)T} n_2 + \vec{t}^{(x_3)T} n_3$$

$$\vec{t}^{(n)T} = [n_1 \ n_2 \ n_3] \begin{Bmatrix} \vec{t}^{(x_1)T} \\ \vec{t}^{(x_2)T} \\ \vec{t}^{(x_3)T} \end{Bmatrix} \quad \left. \vphantom{\begin{Bmatrix} \vec{t}^{(x_1)T} \\ \vec{t}^{(x_2)T} \\ \vec{t}^{(x_3)T} \end{Bmatrix}} \right\} \begin{array}{l} \text{Cauchy} \\ \text{stress} \\ \sigma \end{array}$$

$$\vec{t}^{(n)T} = \hat{n}^T \sigma$$

$$\vec{t} = \sigma^T \hat{n} \rightarrow \text{Cauchy stress eqn.}$$

$$t_i = \sigma_{ji} n_j$$

$$\sigma = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} = \begin{bmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{bmatrix}$$

